

# DEVELOPMENTS IN SOUTH AFRICAN SUGAR FACTORY PLANT INSTALLATIONS 1969-1973

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## Abstract

Tables of some installed process equipment in South African factories are given together with comment on developments in plant design during the last four seasons.

## Introduction

In 1969 an inventory of installed plant was published<sup>1</sup> and this paper brings this data up to date while drawing attention to developments which have taken place since then. Data is presented using the SI system of units. Thirteen tables are given listing the major items of plant installed in the South African sugar factories at present.

No refinery plant is listed but there are several "back-end" refineries operating and as a result boiler power plant and boiling house capacity must be treated with caution when considering these factories. They are shown below together with the percentage white sugar made (1972/73):

ML	95
PG	70
EN	34
GH	86
SZ	44

Irrigation loads make further demands on boiler and power plant and some factories are supplying small amounts of power to by-product plants. For this reason an "average" power or boiler plant installation is difficult to establish. ML, PG, GD, TS and ME carry large irrigation loads.

The diffuser factories are ML, PG (1973/74) UF (one third of total factory throughput to date) EM, EN and UC. Diffusion plants require, in general, less clarification equipment as the bagasse mat acts as a reasonable filter bed in removing much of the mud and fines associated with dirty cane.

In order to provide the information concerning a milling tandem in a compact way, identical units (and drives) are placed in separate columns not necessarily in their order through the tandem. The mill or drive is identified in each case by the numbers from 1 to 7, immediately above the plant description. The drive details are identified only by the above-mentioned numbers and *not* by the mill (or diffuser) which happens to be printed immediately above it.

Plant capacity has been associated with tons cane per hour in the tables (tons fibre for preparation equipment) and is given solely as an order of magnitude. To relate the throughput of a particular plant item to clear juice, massecuite or purities etc., relevant data for each factory is published by SASTA in an Annual Review of each season.

Installed plant can be confusing, when related to throughput, but data obtained of actual capacity used,

e.g. steam flow, power generation etc., proved to be insufficient to provide comprehensive tables and was for that reason not included.

## Cane preparation

Recently considerable attention has been focused on good cane preparation as a means of improving milling performance. Shredder hammers and grid configurations have been redesigned, more horsepower installed, reversed rotation and swing knives are being used and technical interest is still great in this field. With the use of the overhead anvil plate, what is virtually an inverted shredder has been created. Tongaat have designed a new shredder rotor and housing with resulting improvement in Preparation Index figures and hence milling performance.

That this work has paid dividends needs no emphasising when Amatikulu in 1971, after modifications to its shredder (and feeder rollers) increased its throughput from 250 to 280 tch and reduced its LAJ from 29 to 25 together with a reduction of 1.36 points in final bagasse moisture. This was achieved despite a reduction of 5% in imbibition % fibre.

The installation of rubber belt conveyors for prepared cane to replace traditional slat conveyors at a much lower capital and eventual maintenance cost is finding favour. After Jaagbaan's first installation in 1966 several installations have been made recently; at Tongaat, Amatikulu and Pongola, after the shredder and at MV, UF and PG from the cane knives to the shredder. These conveyors do not include the conventional short centre flat belts found under magnetic tramp iron separators. Gledhow and Tongaat use 2.1 m belts for cane transport in the caneyard.

## Direct cane sampling

Soon direct cane sampling installations (including laboratories) will have been installed at all factories by the Central Board. Shredded cane is sampled from automatically-timed full width hatches which allow bulk samples to fall into suitable preparatory equipment for subsampling and analysis. The rejected portion of the cane sample is returned to the carrier. A major significance of these installations is that cane sampling no longer restricts extraction technology to having a crushing unit to provide first expressed juice samples. Cane diffusion is now possible (that is, in contrast to bagasse diffusion) and Hulett's Sugar Corporation has wasted no time in making use of this fact with the proposed Amatikulu cane diffuser for 1974.

## Mills

Gledhow has converted its chain driven feeder rollers to gear drives after extensive alterations to

CANE PREPARATION												
	K = Cane knives	A = Overhead anvil plate	E = Electric motor		300kW = 402 HP.	S = Shredder	R = Reverse Rotation	+ = Coupled motors	T = Steam turbine	LK = Leveller knives		
Factory	Carrier Width mm	Set/Shred-der	Power kW	Drive	Speed rpm	Blades/Ham-mers No.	Swept Diam. mm	Clearance mm	Hammer Mass kg	Total Power kW	Power/Fibre kW/tfh	tfh
ML	2 134	1K 2KRA	447+447 447+447	E E	600 600	44 88	1 854 1 854			1 788	53,9	33,2
PG	2 134	1KRA S	895 895	T T	750 1 200	88 99	1 829 1 320	10 5	10	1 790		19,6
UF1	2 134	LK 1K 2KRA	149 336 328	E E E	— 495 738	12 50 56	1 524 1 905 1 600	254 13		1 298	60,4	21,5
UF2	1 676	S 1K 2KRA	485 186 186	T E E	1 000 735 735	400 64 48	1 346 1 549 1 623	254 25	4	633	56,0	11,3
EM	2 134	S	261	E	960	300	1 270		2	1 500	45,7	32,8
FX1	1 676	LK 1K 2K	150 335 245	E E E	720 735 735	30 36 64	1 574 1 524 1 400	400 62 30		1 325	80,0	16,6
FX2	1 524	S	595	E	982	88	1 270		16	854	70,6	12,1
EN	1 219	1K 2K S	89 111 111	E E E	550 600 975	44 66 64	1 829 2 134 1 066	203 25 431	311	45,7	6,8	
AK	2 134	LK 1KRA *2KA	186 750+750 750	E T T	585 600 600	22 88 48	1 524 2 413 2 134	1 067 203/38A 12	6,5	3 750	85,2	44,0
DK	1 676	S 1K 2K S	1 864 185 260 223	E E E E	980 750 580 982	164 28 30 312	1 728 1 425 1 525 1 270	8—18 250 20	22	668	63,6	10,5
GD	1 219	1K 2K S	149 89 111	E E E	480 480 1 000	22 44 288	1 879 1 778 1 270	50 13	2	349	56,3	6,2
DL	2 134	1K 2K S	410 450 750	T E T	600 960 1 000	36 36 200	1 574 1 574 1 219	37 25	16	1 610	52,8	30,5
GH	2 134	LK 1K 2KRA	185 335+335 450	E E E	292 490 490	32 108 54	1 978 1 978 1 828	1 370 38 75/6A		1 975	52,9	37,3
MV	1 828	1K 2K S	149 186 223	E E E	600 600 983	36 88 328	1 524 1 524 1 270	250 20	4	558	47,3	11,8
JB	2 134	1K 2K S	447 447 521	E E E	593 593 960	40 64 408	1 524 1 524 1 219	216 13 5	4	1 415	47,8	29,6
UC	1 828	1KR 2K	201 398	E E	600 600	32 64	1 630 1 480	25 25		599	74,9	8,0
TS1	2 134	LKR	135+135	E	540	36	1 371	500		1 796	61,7	29,1
TS2	2 134	1KR 2K S	260 260 895	E E T	600 600 1 200	66 78 188	1 524 1 524 1 524	250 25	17	1 190	79,9	14,9
ME	2 134	LK 1K 2K S	56 280 450 1 120	E E E E	490 590 960 960	22 42 42 200	1 321 1 524 1 879 1 270	1 041 406 25	17	1 906	68,6	27,8
IL	1 828	1K 2K 3K S	75 223 260 335	E E E E	613 590 590 960	32 32 64 240	1 524 1 524 1 524 —		16	893	58,4	15,3
RN	1 625	1K 2K S	111+92 186 223	E E E	580 580 970	38 60 320	1 447 1 447 1 219	150 13	7	612	52,8	11,6
SZ	2 134	1K 2K S	447+164 447 1 850	E E T	590 590 1 500	40 80 216	1 524 1 448 1 524	230 12 10	2	2 908		36,8
UK	1 828	1K 2K S	550 223+223 559	T	580 580 1 000	56 64 352	1 346 1 270 1 219	—	17	1 550	69,0	22,5
									2/3			

\*Anvil plate under knives.

## KEY TO TABLE ARRANGEMENT

ML 1,2 (Dewatering)	Mill unit no.
2 134 × 1 067	Roll length × diameter
38 40°	Groove pitch × angle
5R 1 067	Feeder roll type × diameter
1,2	Mill unit no.
T 559	Type of drive, power kW
31 4 500	steam press. bar × rpm or / voltage × rpm

## MILLING TANDEMS AND DRIVES ABBREVIATIONS AND FEEDER ROLL DESCRIPTION

LFR	Fabricated feeder roller
HFR	Cast feeder roller
4R	Pinion driven feeder roller
5R	Pressure feeder mill
6R	AK No. 1 mill has 2 extra feed rollers
E	Electric motor
H,V	Horizontal / Vertical steam engine
T	Steam turbine

## METRIC CONVERSIONS

METRIC CONVERSIONS			
Roll lengths and diameters			
in.	mm	in.	mm
84	2 134	42	1 067
78	1 981	40	1 016
72	1 829	38	965
66	1 676	36	914
60	1 524	34	864
54	1 372	33	838
48	1 219	32	813
44	1 118	30	762
		28	711

Factory tch	Units of different design are listed in separate columns					Factory tch	Units of different design are listed in separate columns				
ML 225	1,2 (Dewater.) 2 134 x 1 067 38 40° 5R 1 067 1,2 T 560 31 4 500	Diffuser				GH 242	1-2 2 134 x 1 118 63 35° 4R 840 1-7 T 480 27 5 700	3-7 2 134 x 1 118 50 35° 4R 840			
PG (150)	1 2 134 x 1 118 50 40° 4R 838 1,7 T 450 11 5 700	2-6 1 676 x 864 50 40° LFR 685 2 H 225 7 70	7 2 134 x 1 118 50 40° 4R 838 3/4, 5/6 H 300 7 70	(Diffuser will by-pass Nos. 2-5)	MV 77	1 1 829 x 965 50 55° LFR 762 1 T 335 16 4 500	2,3 1 676 x 890 38,50 45° LFR 610 2/3, 4/5 H 410 7 60	4 1 829 x 864 50 55° LFR 686	5 1 829 x 864 38 45° LFR 686		
UF1 161	1-6 2 134 x 1 016 50 45° HFR 991 1-6 V 320 11 420	7 2 134 x 1 016 50 45° 5R 863 7 T 370 17 4 500			JB 200	1-6 2 134 x 1 194 50 45° HFR 838 1 E 710 6 600 1 470	2-6 E 650 6 600 1 475				
UF2 80	1,2 1 676 x 864 50 45° LFR 838 1 H 140 7 60	Diffuser 2 H 140 7 60	3 1 676 x 864 50 45° LFR 813 2/4 T 370 9 4 000	4 1 676 x 864 38 45° LFR 838	UC 60	1 1 981 x 914 25 45° HFR 762 1 T 280 17 5 000	Diffuser 2,3 T 205 17 4 500	2,3 1 524 x 762 38 45° LFR 762			
EM 203	1 2 134 x 1 118 50 41° 4R 926 1 T 410 30 5 000	Diffuser 2,3,4 T 410 13 5 000	2 2 134 x 1 118 50 41° 4R 926	3,4 2 134 x 1 118 50 50° 4R 926	TS1 195	1 2 134 x 965 50 45° 5R 940 1 T 560 14 4 000	2-6 2 134 x 965 50 45° LFR 914 2-6 V 335 14 420	7 2 134 x 965 25 35° 5R 813 7 T 450 14 4 000	7 2 134 x 965 25 35° 5R 813 7 T 450 14 4 000		
FX1 111	Crusher 1 829 x 927 50 40° LFR 686 Crusher 1/2 H 300 7 60	1,3 1 676 x 927 50 40° LFR 610 1/2 E 300 3 300 735	2,4,5,6 1 676 x 927 50 40° LFR 533 3/4/5 E 450 3 300 735	6 H 300 7 60	TS2 98	1 2 134 x 1 067 25 35° 5R 1 067 1 T 560 14 4 000	2-6 1 676 x 914 50 45° LFR 762 2/3 T 335 14 4 000	4 H 260 7 50	5/6 V 280 11 350		

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MILLING TANDEMS AND DRIVES

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mill cheeks. The pinions and gears ( $\pm 1,6$  m diam.) are fabricated from five flame cut plates, each about 50 mm thick riveted together, to form a single gear. This factory has had excellent results using white metal mill bearings on cast iron housings. Amatikulu has installed a pressure feeder unit to its first mill driven by hydraulic motors mounted within the rollers. Hydraulic motors are also utilized in the Saturne diffuser dewatering rollers and final mill drive.

Mill grooving has moved away from  $55^\circ$  down to between  $45^\circ$  and  $40^\circ$ .

The use of scraper plates with cast teeth has been accepted generally.

Gledhow are successfully running slat type inter-carriers without tail shafts and sprockets by simply

guiding the chains round semi-circular runner strips. Union Co-op has used some experimental high density plastic rollers instead of stainless steel in their slat conveyor feeding the diffuser.

### Diffusers

A Saturne flooded diffuser was installed at Umfolozi in 1971. The unit is an annular box (12 m OD  $\times$  9 m ID  $\times$  4 m wide) designed to handle 150 tch. A series of carrier arms on a massive annular beam 1,5 m deep carries the bagasse through three quarters of a full circle while moving in a counter current juice stream. The drive is by a hydraulic piston.

An experimental single cell Fletcher and Stewart diffuser, after rigorous testing at Empangeni, is

### DIFFUSERS

Factory	Make	Design throughput tch	Effective screen area m <sup>2</sup>	Length m	width m	Outside diam. m	Inside diam. m	Cane crushed tch
ML	De Smet	225	160	33,2	7,0			225
PG	Fletcher & Stewart 5 cells	150		—	—			N.A.
UF	Saturne	150			4	12	9	80
EM	BMA 1 F & S cell	225	170	35,4	4,8			203
EN	De Smet	90	59	73,6	2,49			48
UC	BMA	108	48	28	2,2			60

### JUICE HEATERS

Heating surface in m<sup>2</sup>       $100m^2 = 1076$  ft<sup>2</sup>  
Not including Liquid to Liquid Heaters

Factory	Primary No. H.S.	Secondary No. H.S.	Diffuser No. H.S.	Pre-evaporator No. H.S.	Total H.S. m <sup>2</sup>	Total m <sup>2</sup> /tch
ML	5 232		5 232	2 232	2 784	12,39
PG	9 93		1 300**		1 137	8,70
UF	4 139	2 232	3 93	2 167	2 245	9,71
		2 167				
		1 278				
EM	4 790		3 = 598	4 = 392	1 780	8,8
FX	1 325**	2P/S 136		2 136	1 141	6,25
		2 136				
EN	1 111	1 111	6 50	1 93	615	12,75
AK	3 204	3 204		3 204	1 836	6,00
DK	2 93	1 167		1 186	539	7,47
GD	2 93				278	6,42
	2 46					
DL	4 = 808			2 186	1 180	5,67
GH	10 186			2 209	2 278	9,40
MV	3 93					
	1 139					
JB	3 232	4 232		1 232	418	5,43
UC	2 93		2 186	1 93	1 856	9,30
TS	3 175	4 186			465	7,80
	3 186				1 827	6,24
ME	2 232	3 232			1 160	6,2
IL	2 102	1 186			664	6,28
	1 186	1 88*				
RN	1 204	2 149			919	12,23
	3 139					
SZ	7 204			2 697	2 822	11,61
UK	4 111	2 214			872	5,49

\* not used

\*\*7m long tubes

achieving full operational status with a five cell installation (behind a single mill) at Pongola, due to be commissioned in August 1973: this mill cum diffuser will initially handle 150 tch. These units have a double perforated deck with chain driven slats moving the bagasse at about 3 m/minute, first down and then up the inclined decks under continuous sprays of recirculated juice. The bagasse blanket is about 0,5 m deep and is allowed to fall freely at each transfer point.

Compared with a milling tandem of equal capacity diffusers have three highly desirable characteristics, lower capital cost, high extraction and lower maintenance costs. Amatikulu is scheduled to install a cane diffuser for the 1974 season and a number of powerful mills will become redundant. One can foresee that pairs of these units (as dewatering mills) combined with other cane diffusers will be replacing existing old milling tandems very shortly. Not only will this reduce the maintenance costs associated with obsolescent plant but it can also provide a generous reserve of extraction plant capacity.

#### Juice heaters

Felixton and Pongola will each have a vertical

heater with tubes 7 m long this season. This is a logical step to reduce capital cost and cleaning time.

#### Clarifiers

A 50% reduction in retention time has been achieved with slight modifications to existing Rapidorr clarifiers. An increase in the number of take-off points has resulted in clear juice being removed at double the previous rates possible with three or four off-take points. Three very large single clarifiers, 11 m in diameter, have been installed at Empangeni, Darnall, and Umzimkulu.

By using gravity mud take-off points, the use of mud pumps is being slowly discontinued. Tests are proceeding with pilot plant models of new clarifier designs and a full scale trayless clarifier is being built at Empangeni for commissioning this season.

#### Evaporators

The number of long tube (4 to 7 m) evaporators has increased from 8 to 13 during the period under review. The later vessels have all utilized a separate

#### CLARIFIERS

$200 \text{ m}^3 = 7063 \text{ ft}^3$

G = Graver  
B = Bach

D = Dorr multifeed  
BMA = BMA

R = Rapidorr  
R4 = Rapidorr 444

Factory	No.	Make	Diam m	Capacity m <sup>3</sup>	Total	Capacity/tch
ML	1	G	9,8	441,7	441,7	1,97
PG	2	D	6,1	= 291,6	804,1	6,15
	1	R	6,7	220,9		
UF	1	R	7,3	263,3	1 049,3	4,49
	1	R	7,9	369		
	1	B	6,7	171		
	1	B	6,1	125		
	1	B	5,4	121		
EM	1	R4	11,0	460,0	723,3	3,60
	1	R	7,3	263,3		
FX	1	D	5,5	147	557,0	3,05
	1	R	5,5	147		
	1	R	7,3	263		
EN	1	R	6,1	181,2	181,2	3,76
AK	4	R	7,3	= 1 050,6	1 050,6	3,43
DK	1	G	6,1	127,0	274,0	3,80
	1	R	5,5	147,0		
GD	1	B	4,9	68,0	249,2	5,82
	1	R	6,1	181,2		
DL	1	BMA	11,0	460,0	460,0	2,21
	3	B**	6,1	= 375,0		
GH	1	R	8,5	356,8	781,6	3,22
	2	D	7,3	= 424,8		
MV	2	D	5,5	= 294,5	294,5	3,82
JB	2	R	9,8	= 931,6	931,6	4,67
UC	1	BMA	4,0	25,5	206,7	3,50
	1	R	6,1	181,2		
TS	3	B	6,7	= 456,6	980,5	3,35
	2	R	7,3	= 523,9		
ME	3	R	7,3	= 787,2	787,2	4,23
IL	1	D	6,7	177,8	441,1	4,17
	1	R	7,3	263,3		
RN	1	D	6,1	147,2	263,3	3,50
	1	R	4,9	116,1		
SZ	2	D	6,7	= 356,8	767,4	3,15
	1	R	9,1	410,6		
UK	1	R4	11,0	460,0	460,0	2,90
	2**	B	4,3	= 98,3		

\*\* Not in use.

## EVAPORATORS

500 m<sup>2</sup> = 5 382 ft<sup>2</sup>

Factory	Heating surface in m <sup>2</sup> effect numbers					Total H.S.	H.S./tch
	1	2	3	4	5		
ML	1 579 1 022 1 022	1 022 1 022	743	743		7 153	31,8
PG	929 1 115	465 465	465 465	465 465		4 834	37,0
UF	1 858 836	1 114 930 348 <sup>2</sup>	670 <sup>1</sup> 557 348 <sup>2</sup>	670 557 348 <sup>2</sup>	670 557 348 <sup>2</sup>	8 419	36,4
EM	1 013 848	710 552	710 343	710 343	710** 343	6 280	30,9
FX	1 400 700	1 160	780	780	650 650	6 120	33,5
EN	743	232	232	325	325	1 857	38,5
AK	1 858 743 743	743 743	743 743	743 743 743		9 288	30,3
DK	279 418	143 325	143 325	143 325		2 101	29,1
GD	372 116	279	232	116 116		1 231	28,7
DL	1 394 1 394	817 437	817 437	817 437	817 437	7 804	37,5
GH	2 787 2 787	1 394 929	1 394	929 650		10 870	44,8
MV	870	216 181	216 181	216 181	321 321	2 703	35,1
JB	1 394 1 394	1 210	1 210	1 210		6 418	32,2
UC	836	279	279	279		1 673	28,1
TS	2 230 2 230 929 929	557 372 557	557 372 557	557 372 557	557 372 557	12 262	41,9
ME	2 508 275	929 275	743 275	743	743	6 491	34,9
IL	929	557	557	279 279		3 475	32,9
	279	279	158	158			
RN	697	348 186	348 186	348 186	348 186	2 833	37,7
SZ	1 394 929 929 929	650 348	650 348	650 348	650 348	8 173	33,5
UK	1 208 603 860	(Vapour cell) 416 574	416 574	416 574		5 641	35,5

<sup>1</sup>An extra 670 is spare<sup>2</sup>Not in use and not included in total H.S.

\*\*Internal condenser

entrainment separator vessel to facilitate cleaning operations by making the cover plate of the tube vessel firstly hinged and now completely removable by means of a bayonet type locking device. These ends and joints are designed to withstand 0,5 bar pressure of bled vapour for pan boiling and juice heating.

Both new Kestner pre-evaporators at Tongaat have a built-in heater involving an up and a down pass of a group of evaporator tubes. The need for a clear juice heater is thus eliminated. These two vessels are tubed with stainless steel tubes, one in Type 304 and the other in Type 430.

#### Vacuum pans

The installation of a built-in tray type barometric condenser in the vapour space of a pan is such a logical move that one can only wonder why it was not used years ago. The first pan was designed by Hulett and installed at Darnall.

Two 85 m<sup>3</sup> pans have been installed recently, one at Amatikulu and one at Gledhow. The downtake diameters are about 3 m and 100 mm diameter tubes have been used with a length of 800 mm.

A 42 m<sup>3</sup> A pan has been installed at Felixton on a self-supporting circular column which acts as a

strike receiver for other pans as well. No grain segregation is reported.

#### Crystallizers

There has been a trend to operate crystallizers in series and these are shown in the plant table being marked with an "S" where applicable. Large gutters have been installed to ensure a series flow from vessel to vessel and a midway baffle ensures no short circuiting of massecuite flow across the top of the crystallizers.

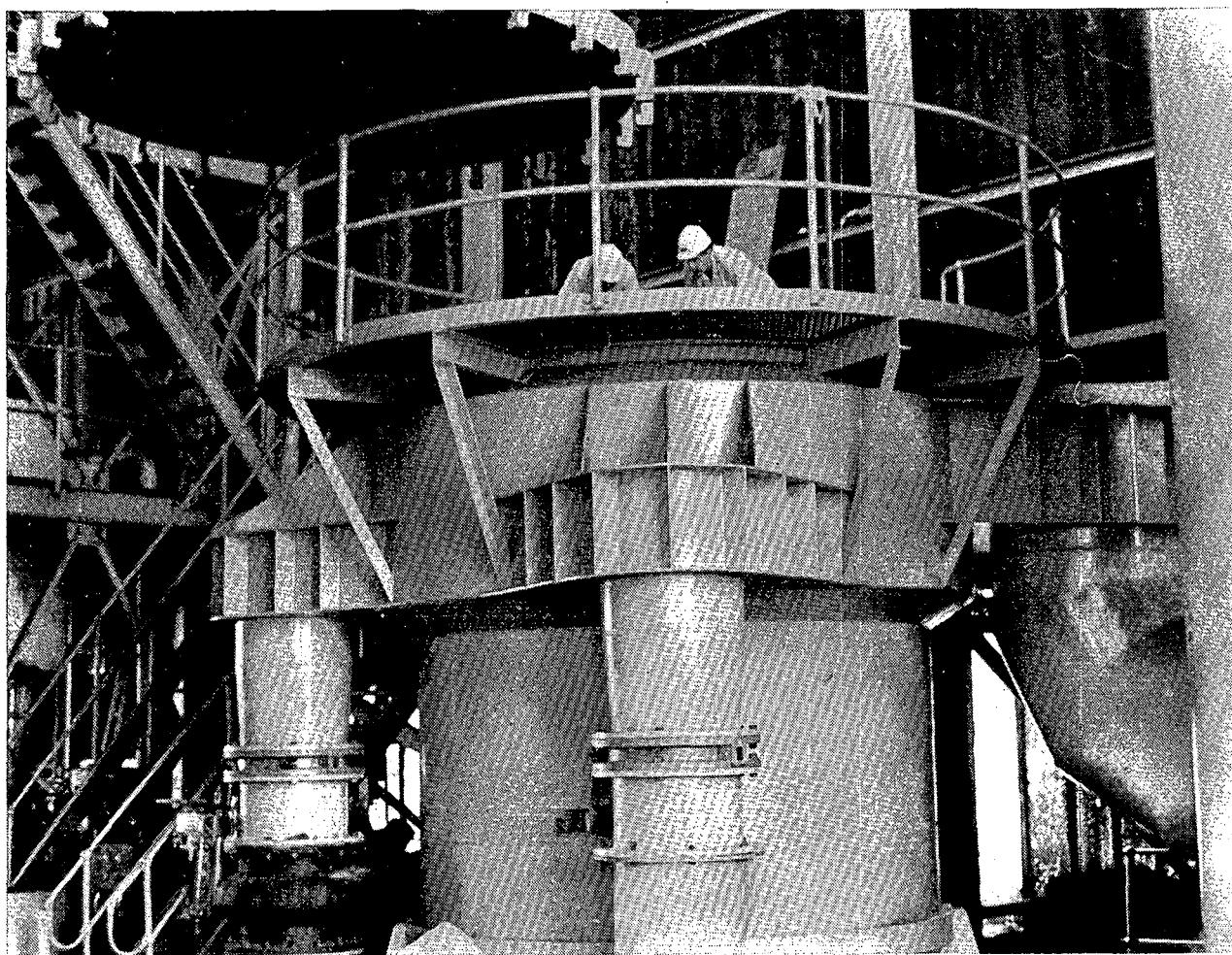
Drive of crystallizers by means of hydraulic pistons and suitable drive wheels together with finned tube cooling elements have been installed at some mills.

Gledhow is installing a common 170 m<sup>3</sup> strike receiver under its A pans this coming season.

Malelane is utilizing the series flow principle to solve a massecuite transport problem from pans to C centrifugals.

A new design of two vertical crystallizers utilizing a U-shaped flow pattern with two vertical vessels is being built for Renishaw C massecuites.

Reheating of C massecuite is still being carried out by fin-tube elements carrying heating water. Electric reheaters are not popular and only three are working,



Long tube evaporator at Amatikulu showing end cover removed for access to tube sheet. Steam inlets are shown at left and centre, with vapour outlet main and entrainment separator just visible at right.

## ROTARY VACUUM FILTERS

E = Eimco

OC = Oliver Campbell

50 m<sup>2</sup> = 538 ft<sup>2</sup>

Filters 2,44 m diam.

Factory	No.	Make	Length m	Area m <sup>2</sup>	Total area	m <sup>2</sup> /tch
ML	2	E	4,9	37,2	74,4	0,33
PG	2	OC	4,9	37,2	74,4	0,57
UF	3	OC	3,7	27,9	139,5	0,60
	2	E	3,7	27,9		
EM	3	OC	4,9	37,2	148,8	0,73
	1	E	4,9	37,2		
FX	5	OC	3,7	27,9	139,5	0,76
EN	1	OC	3,7	27,9	46,5	0,96
	1	E	2,4	18,6		
AK	4	OC	4,9	37,2	148,8	0,49
DK	2	OC	2,7	20,9	55,6	0,77
	1	OC	1,8	13,8		
GD	1	E	3,7	27,9	27,9	0,65
DL	4	OC	3,7	27,9	111,6	0,54
GH	5	OC	4,9	37,2	186,0	0,77
MV	2	OC	3,7	27,9	76,7	1,00
	1	OC	2,7	20,9		
JB	1	OC	4,9*	65,0	102,2	0,51
	1	OC	4,9	37,2		
UC	1	E	4,9	37,2	37,2	0,62
TS	5	OC	3,7	27,9	167,4	0,57
	1	E	3,7	27,9		
ME	4	OC	3,7	27,9	111,6	0,60
IL	2	OC	3,7	27,9	55,8	0,53
RN	1	OC	4,3	32,5	51,1	0,68
	1	OC	2,4	18,6		
SZ	4	OC	4,9	37,2	148,8	0,61
UK	2	E	3,7	27,9	83,7	0,53
	1	OC	3,7	27,9		

\*Filter is 4,27m in diam.

## PAN STORAGE TANKS

100 m<sup>3</sup> = 3 531 ft<sup>3</sup>

Factory	Capacity in m <sup>3</sup>			Total	Seed Receivers Magma Mixers No.	Cap. each m <sup>3</sup>
	Syrup	A mol.	B mol.			
ML	228	91	91	410	6	19,8
PG	261	102	113	476	1	17,0
					1	23,0
UF	139	87	71	297		
EM	246	104	104	454	2	25,5
					1	34,0
FX	116	82	85	283	3	28,3
EN	—	—	—	—	2	4,0
					2	8,5
AK	107	86	86	279	3	48,0
DK	68	57	47	172	2	14,0
			—		1	8,5
GD	42	73	73	188	1	13,0
					1	8,5
DL	159	82	68	309	1	12,7
					2	56,0
GH	286	166	117	569	1	56,0
					2	30,0
MV	62	62	62	186	6	13,0
JB	200	100	100	400	6	31,1
					3	25,5
UC	65	43	33	138	1	20,0
TS	145	66	60	271	1	17,0
					1	22,7
ME	102	102	102	306	1	26,9
					1	—
IL	—	—	—	—	—	—
RN	119	93	61	273	1	10
					1	17
SZ	317	159	238	714	1	34
					1	42
UK	132	88	88	308	1	34

all at Entumeni. The two techniques should be used together.

### Centrifugals

Continuous machines have virtually made a clean sweep in the curing of C massecuites. Throughputs of 1 m<sup>3</sup> per hour are being achieved compared with 1,8 m<sup>3</sup> in Australia and Mauritius. The massecuite viscosity ranges are similar despite popular opinion that ours are above their ranges. Whether viscosity is the sole criterion for this comparatively lower throughput remains an open question, but it is one which is also related to recovery.

There are many B continuous machines in service

and even with crystal breakage these B sugars are being used as magma for the footings of A boilings.

Umfolozi installed a battery of 6 batch machines to handle their low grade products.

### Sugar driers

A new Roto-louvre type sugar drier driven by motor tyre type suspension, doing away with the noisy rollers and gear or chain drive, has been installed at Jaagbaan.

### Boiler plant

The only major installation in this department has been at Tongaat, where a 36 000 kg/h Thomson

### VACUUM PANS

Factory	No.	A Cap. m <sup>3</sup>	H.S. m <sup>2</sup>	No.	B Cap. m <sup>3</sup>	H.S. m <sup>2</sup>	No.	C Cap. m <sup>3</sup>	H.S. m <sup>2</sup>	Total Capacity	Capacity m <sup>3</sup> /tch
ML	3	42,3	237	2	42,3	209	1	42,3	181*	338,4	1,5
	1	42,3	181*		1	31,1		1	42,3		
PG	1	34,0	214	1	31,1	197	1	31,1	197	221,1	1,7
	2	31,1	197		1	22,7		1	22,7		
UF	1	45,3	269	1A/B	45,3	278	1	22,7	149	339,5	1,5
	2	36,8	223		1	42,3		2	45,3		
EM	1	42,3**	252	1	22,6	148	1B/C	42,4	223	302,6	1,5
	1	51 **	325		1	51		1	22,7		
FX	1	51	288	1	51	302	1B/C	42,3	223	255,0	1,4
	2	42,5**	250		1	42,5**		1	42,3		
EN	1	34,0	177	1	25,5*	153	1	12,7*	70	113,0	2,3
	1	25,5	130		1	25,5*		1	8,5		
AK	1	25,5	158	1	25,5*	134	2	42,3**	216	381,1	1,2
	3	42,3	251		2	42,3**		2	42,3**		
DK	1	85**	511	2	12,7	67	1	26,6	153	109,9	1,5
	3	19,3	136		3B/C	9,1		1	26,6		
GD	1	20,4		1	28,3	167	1	28,3	177	284,8	1,4
	1	22,7			1	28,3		1	28,3		
DL	1	51,0**	268	1	28,3	177	1	28,3	167	113,0	2,3
	1	50,0			1	28,3		1	28,3		
GH	1	85**	488	3	36,8	223	3	36,8	223	418,8	1,7
	2	56,5	372		1	36,8		1	36,8		
MV	1	34,0	173	1	34,0	150	1	34,0	150	161,4	2,1
	2	17,0	67		1	12,7		1	12,7		
JB	2	12,7	37	1	31,1		1	31,1		232,0	2,2
	4	42,3	251		1	42,3		1	34,0		
UC	2	25,5	147	1	25,5	147	2	42,3	209	102,0	1,7
	6	28,3	145		3	28,3		3	28,3		
TS	2	51**	318	1	45,3	295	4	28,3	121	339,6	1,2
	1	43,9	253		1	45,3		4	28,3		
ME	2	28,3		1	31,1		1	31,1		349,7	1,9
	2A/B	31,1			1	34,0		1	34,0		
IL	2	12,7	37	1	17,0		1	17,0		118,6	1,6
	2	12,7	37		1	17,0		1	17,0		
RN	2	24,9**	111	1	22,7	111	1	24,9	111	341,8	1,4
	1	21,2	93		1	22,7		1	21,2		
SZ	4A/B	42,3	223	2	28,3	158	3	28,3	158	257,9	1,6
	2	42,5	223		1B/C	42,5		1	42,5*		
UK	1	22,7	195	1B/C	42,5	223	1	22,7	139	257,9	1,6
	1	22,7	195		1B/C	42,5		1	22,7		

\* Stirrer equipped pan  
\*\* Internal condenser

ft. <sup>3</sup>	m <sup>3</sup>
2 000	56,6
1 600	45,3
1 500	42,3
1 200	34,0
1 000	28,3
800	22,7
600	17,0

boiler was installed in 1971 to replace three old Stirling boilers. This unit has a Thomson furnace based on the Jaagbaan design and has a generous capacity for overload. Tongaat uses belt conveyor bagasse transport in the boiler house and has installed highly effective vibrating screen units for the recovery of bagacillo for byproduct use.

There will be seven flue gas scrubbers in operation this season and each year more will be installed until all stacks can meet the particle emission level of 450 mg/m<sup>3</sup>.

#### Power generating plant

Doornkop installed a new turbo-alternator and standby diesel plant.

#### Water pollution

Various types of water purification plant including biofilters, aerobic and anaerobic ponds, spray irrigation schemes, etc. have been installed to return purified or semi-purified water to the river or lands. Umfolozi has installed two Paasveer ditches, one for sewage and one for factory waste water which comply fully with the provisions of the return water specifications.

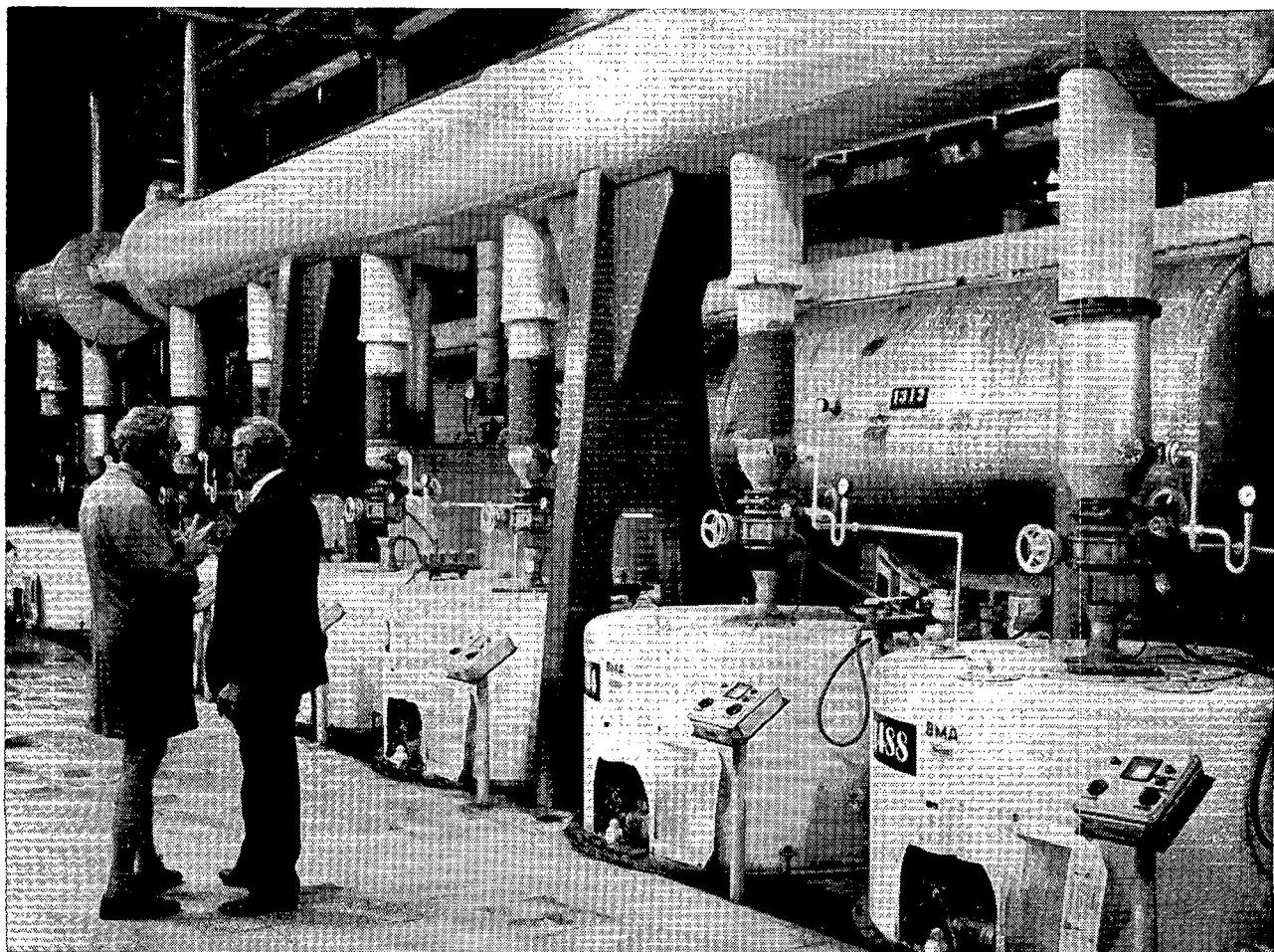
#### Factory nomenclature

A key to the factory code letters used in the tables is given below. The listing is in geographic order from North to South.

ML	Malelane	GH	Gledhow
PG	Pongola	MV	Melville
UF	Umfolozi	JB	Jaagbaan
EM	Empangeni	UC	Dalton (Union Co-op)
FX	Felixton	TS	Tongaat
EN	Entumeni	ME	Mount Edgecombe
AK	Amatikulu	IL	Illovo
DL	Darnall	RN	Renishaw
DK	Doornkop	SZ	Sezela
GD	Glendale	UK	Umzimkulu

#### Conclusions

Cane preparation, milling versus diffusion and shorter clarification periods are under close scrutiny, continuous pan boiling and high grade centrifuging are somewhat further off but improvement in low grade centrifuging capacity is an immediate requirement. Replacement of existing plant, costly in maintenance, by reliable virtually maintenance-free equipment must be the final objective. Before long, the



Battery of continuous machines at Sezela illustrating continuation of clean lines and spacious layout which was started with the Darnall 'C' station.

shortage of natural fibre in this country may necessitate substitution of coal for bagasse in our boiler plant while the fibre is used in byproducts. High thermal efficiency in processing will be our next priority and vapour 3 bleeding must no longer be left to the distant realms of beet sugar technology.

It is gratifying to see that more attention is being paid to the broader principles of unit process technology rather than the well-tried but rather narrow so-called sugar engineering of the past.

### Acknowledgements

Thanks are extended to all factory and central technical personnel for their co-operation in supplying gaps in the published data and to Mr. P. de Robillard (SMRI) for his willing assistance in compiling the tables.

### REFERENCE

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### CENTRIFUGALS

Factory	A					B				
	Make	No.	Speed rpm	Diam. mm	Depth mm	Make	No.	Speed rpm	Diam. mm	Depth mm
ML	WS	5	1 000	1 372	1 016	WS Co	4	2 200	864	34°
	?	1		1 340	830	B	4	1 500	1 067	762
PG	B	5	1 500	1 067	762	WS	4	1 500	1 220	762
UF	WS	10	1 500	1 220	762	BMA Co	4	2 200	850	
EM	B	8	1 200	1 220	762	BMA Co	3	2 200	850	
FX	B	5	1 500	1 220	762	WS Co	1	2 200	865	
EN	B	3	1 500	1 067	762	B	1	1 500	1 067	762
						B	2	1 500	1 067	610
AK	B	14	1 500	1 220	762	BMA Co	6	2 200	850	
DK	WS	3	1 450	1 016	762	WS	2	1 450	1 016	762
GD	ASEA	1	1 200	1 220	762	WS	1	2 200	1 220	762
DL	B	7	1 500	1 220	762	BMA Co	4	2 200	850	
GH	B	13	1 000	1 220	762	BMA Co	6	2 200	850	
MV	B	3	1 500	1 067	762	B	3	1 500	1 067	762
JB	BMA	6	1 450	1 220	762	BMA	6	1 450	1 220	762
UC	B	2	1 500	1 067	762	B	3	1 500	1 067	762
TS	ASEA	8	1 300	1 220	762	AC Co	1	2 200		
ME	B	9	1 500	1 067	610	BMA Co	6	2 200	850	
IL	PC	1	—	1 067	762	HL Co	5	2 200	582	34°
	WS	4	1 500	1 016	762	BMA Co	4	2 200	850	
RN	B	4	1 500	1 067	762	WS	4	1 400	1 067	762
SZ	B	4	1 500	1 220	762	B	3	1 500	1 067	762
	BMA	2	1 500	1 340	830	B	5	1 500	1 220	762
UK	B	5	1 500	1 067	762	B	3	1 500	1 067	762
	WS	1	1 000	1,200	762					

in.      mm

54	1 472	Co = Continuous
48	1 220	AC = Allis Chalmers
42	1 067	ASEA = ASEA
40	1 016	B = Broadbent
34	864	BMA = BMA
30	762	PC = Pott Cassels & Williamson
24	610	WS = Western States Machine Co.
		HL = Hein Lehmann

CENTRIFUGALS (*continued*)

Factory	Make	C. Foreworkers			C Afterworkers					
		No.	Speed rpm	Diam. mm	Depth mm	Make	No.	Speed rpm	Diam. mm	Depth mm
ML	WS Co	8	2 200	864	34°					
	? Co	3	2 200							
PG	B	8	1 500	1 067	762	B	2	1 500	1 067	762
UF	WS	6	1 500	1 372	1 016	AC Co	4	2 200		
EM	BMA Co	12	2 200	850		BMA Co	3	2 200	850	
FX	B	16	1 500	1 067	610	B	3	1 500	1 067	610
EN	B Co	3	1 800	36	30°					
AK	BMA Co	15	2 200	850		BMA Co	6	2 200	850	
DK	WS	4	1 350	1 016	762	HL Co	2	1 500	762	30°
	WS Co	1	2 200	864	34°					
GD	WS Co	2	2 200	864	34°					
DL	BMA Co	10	2 200	850		BMA Co	4	2 200	850	
GH	BMA Co	12	2 200	850		WS Co	3	2 200	864	
						BMA Co	1	2 200	850	34°
MV	WS Co	4	2 200	864	34°					
JB	BMA	11	1 720	1 220	762	BMA Co	3	1 750	1 000	
	BMA Co	3	2 200	850						
UC	AC Co	4	2 200	800	475					
TS	BMA Co	15	2 200	850						
ME	B	3	1 500	1 067	610	B	5	1 000	1 067	610
	ASEA	6	1 700	1 220	762					
IL	ASEA	4	1 800	1 220	762	WS Co	2	2 200	865	34°
	WS	2	1 700	1 016	762					
RN	B	3	1 500	1 067	762	B	1	1 500	1 139	762
SZ	BMA Co	12	2 200	850		BMA Co	3	2 200	850	
						WS Co	2	2 200	865	
UK	WS Co	10	2 200	865	34°	AC Co	1	2 200	686	34°

in.	mm
54	1 472
48	1 220
42	1 067
40	1 016
34	864
30	762
24	610

Co = Continuous  
 AC = Allis Chalmers  
 ASEA = ASEA  
 B = Broadbent  
 BMA = BMA  
 PC = Pott Cassels & Williamson  
 WS = Western States Machine Co.  
 HL = Hein Lehmann

## CRYSTALLIZERS

W = Water cooled

S = Series connected

Cap. in m<sup>3</sup>

Factory	No.	A Cap.	No.	B Cap.	No.	C Cap.	Total	Cap/ tch
ML	8	42,3	1	108	1	108		
PG	6	17,0	4S	42,3W	12S	42,3W	1 231,2	5,48
UF	4	45,3	7	17,0	20	17,0W		
	8	25,4	10	25,4	6	31,1W	747,6	5,72
EM	8	30,8	13	30,8	7	25,4	997,4	4,31
FX	1	99,5	9	14,2	4	45,3W		
	1S	56,6			7S	44,0W	954,8	4,70
	3	14,2			8	34,0W	598,5	3,3
EN	2	19,8	5	8,5	5	12,7W	264,6	5,49
	1	17,0	3	25,5	1	25,5W		
AK	12	46,4	8	44,4W	16S	44,4W	1 622,4	5,30
DK	8	9,9	7	12,7	6	28,3W	337,9	4,7
GD	3	20,4	4	9,9	4	9,9	180,0	4,20
					4	9,9W		
DL	5S	28,3	9S	28,3	15S	28,3W	820,7	3,94
GH	3S	56,6	9S	36,8	4S	36,8		
	3S	56,6	3S	36,8	7S	56,6W	1 531,4	6,32
	1	170,0						
	1	36,8						
MV	8	17,0W	2	34,0W	5	34,0W	408,0	5,30
			2	17,0W				
JB	6	42,3	6	42,3W	18	42,3W	1 269	6,36
UC	3	25,5	3	25,5W	5	25,5W	331,5	5,56
TS	5	28,3	7	28,3	8S	28,3W	849,0	2,90
					10	28,3W		
ME	4	28,3	4	28,3	16	28,3W	1 018,8	5,47
	6S	28,3	6S	28,3				
IL	4	34,0	4	34,0	8	34,0W	612	5,79
					2	34,0W		
RN	3S	24,1	4S	24,1	1	48,2	361,5	4,81
					4S	56,6W		
SZ	8	42,3W	8	42,3W	4S	28,0W		
					8S	28,3W	1 353,6	5,57
					8S	28,3W		
UK	3	45	4	45	8S	42,3W	710,2	4,46
	2	22,7						

ft. <sup>3</sup>	m <sup>3</sup>
2 000	56,6
1 600	45,3
1 500	42,3
1 200	34,0
1 000	28,3
800	22,7
600	17,0

### BOILERS

10 bar = 145 psig

B = Bi-drum CTM = Cross-tube marine WIF = Wrought Iron Front S = Spreader D = Dutch Oven T = Thomson C = Cyclone SC = Spray Chamber IS = Scrubber

Factory	No.	M.C.R. kg / h x 1 000	Type	Press. bar	Temp. °C	Heating surfaces				Furnace type	Grit arrestor	Accumulator		Total installed kg / h x 1 000	Installed capacity / tch kg/t cane	
						Convection m <sup>2</sup>	Furnace m <sup>2</sup>	S / H m <sup>2</sup>	Econ. m <sup>2</sup>			No.	Cap. kg/h x 1 000			
ML	3	45	B	31	400	1 228	*	*	270	724	SSSSSSSSSSSS	C	2	11	135	601
	2	23	B	13,8	260	581	*	73,6	—	405		Nil			90	688
UF	4	17	B	11	260	515	*	—	—	358	CCCCCCCCCCCC	Nil	2	11	207	895
	1	57	B	31	400	1 450	153	233	—	976		IS				
EM	2	27	B	13,8	260	650	461	—	—	—	DDDDSSSSSSSS	SC	2	23	155	763
	2	14	CTM**	13,8	260	478	—	—	—	—		SC				
EM	1	14	WIF	11	260	680	—	—	—	—	DDDDSSSSSSSS	SC	2	23	155	763
	2	20	WIF**	11/13,8	260	481	—	—	—	—		SC				
FX	1	14	B	13,8	260	752	—	—	—	228	SSSSSSSSSSSS	SC	2	23	155	763
	1	45	B	31	370	854	*	116	1 261	504		SC				
EN	1	31	WIF	14,3	288	1 031	—*	110	—	—	DDDDDDDDDDDD	SC	2	23	155	763
	1	23	B	13	204	681	—	51	—	—		SC				
EN	4	14	WIF	10	204	681	—	56	—	—	DDDDDDDDDDDD	SC	2	23	155	763
	1	45	B	31	370	854	110	116	1 261	504		C/SC				
EN	1	45	B	13,8	277	967	369	106	—	502	DDDDDDDDDDDD	C/SC	2	23	155	763
	1	16	WIF	7	170	373	—	—	121	185		SC				
AK	1	23	WIF	13,8	200	681	—	—	—	200	DDDDDDDDDDDD	SC	2	23	155	763
	1	23	B	10,3	200	279	—	—	273	388		Nil				
DK	1	23	B	17	330	675	62	51	—	471	DDDDDDDDDDDD	C	2	23	155	763
	4	36	B	31	370	609	* —	95	878	529		Nil				
GD	1	21	B	25	370	744	—	—	—	406	DDDDDDDDDDDD	Nil	2	23	155	763
	1	11	WIF	10	220	257	—	—	—	—		Nil				
GD	3	7	WIF	10	220	229	—	—	—	—	DDDDDDDDDDDD	Nil	2	23	155	763
	1	5	WIF	14	220	229	—	—	—	—		Nil				
DL	1	14	WIF	13,8	316	497	—	—	232	400	DDDDDDDDDDDD	Nil	2	23	155	763
	2	7	WIF	10	185	340	—	—	—	153		Nil				
DL	1	45	B	31	370	854	—	—	126	504	DDDDDDDDDDDD	C	2	23	155	763
	2	32	WIF	13,8	277	1 030	205	—	—	650		Nil				
DL	1	23	WIF	13,8	277	681	153	*	—	664	DDDDDDDDDDDD	Nil	2	23	155	763
	1	23	B	31	345	671	—	—	—	228		Nil				

\*Included in convection surface area.

\*\*Not in use.

BOILERS 2

10 bar = 145 psig

B = Bi-drum CTM = Cross-tube marine WIF = Wrought Iron Front S = Spreader D = Dutch Oven T = Thomson C = Cyclone SC = Spray Chamber IS = Scrubber

Factory	No.	M.C.R. kg / h x 1 000	Type	Press. bar	Temp. °C	Heating surfaces					Furnace type	Grit arrestor	Accumulator		Total installed kg / h x 1 000	Installed capacity/ tch kg/t cane	
						Convection m <sup>2</sup>	Furnace m <sup>2</sup>	S / H m <sup>2</sup>	Econ. m <sup>2</sup>	Air H. m <sup>2</sup>			No.	Cap.kg/h x 1 000			
GH	1	45	B	27,5	370	774	142	137	373	1 560	S	C	2	27	194	800	
	1	45	B	27,5	370	1 106	217	—	—	—		C	—	—	—	—	
MV	1	34	CTM	27,5	370	—	—	—	—	—	D	Nil	—	—	56	727	
	1	34	CTM	27,5	370	—	—	—	—	—		Nil	—	—	—	—	
JB	2	18	WIF	13,8	320	581	—	—	—	—	D	Nil	—	—	—	—	
	1	23	B	17	320	310	* *	142	680	732		Nil	—	—	—	—	
UC	1	14	B	11	300	373	—	85	—	452	S	Nil	—	—	—	—	
	1	7	WIF	10	200	—	—	—	—	—		Nil	—	—	—	—	
TS	2	2	WIF	10	200	118	—	—	—	—	D	Nil	—	—	—	—	
	1	4	WIF	10	200	235	—	—	—	—		Nil	—	—	—	—	
ME	1	4	WIF	7	170	235	—	—	—	—	D	Nil	—	—	—	—	
	3	45	B	31	400	1 779	* *	—	—	1 176	T	Nil	—	—	135	676	
IL	1	23	B	17	282	781	* *	—	196	388	S	C	—	—	—	37	620
	1	14	WIF	11	188	—	—	—	—	—		Nil	—	—	—	—	
RN	1	36	B	14	340	—	—	—	—	—	T	IS	2	24	212	725	
	2	32	WIF	13,8	340	1 030	—	—	—	—		Nil	—	—	—	—	
SZ	1	23	CTM	14	340	—	—	—	—	—	D	IS	—	—	—	—	
	1	27	B	14	340	698	* *	—	—	—		IS	—	—	—	—	
UK	1	9	WIF	11	260	341	—	—	—	—	S	SC	—	—	—	—	
	5	7	5Drum	11	260	372	—	—	—	—		SC	—	—	—	—	
IL	1	27	B	13,8	240	—	—	—	—	487	D	C	2	12,5**	152	816	
	5	25	WIF	13,8	240	770	—	184	—	465		Nil	—	—	—	92	870
RN	1	25	B	31	800	—	* *	—	—	—	D	C	—	—	—	—	
	5	9	WIF	11	445	—	—	—	—	—		Nil	—	—	—	—	
RN	2	11	CTM	13,8	558	—	—	—	—	—	D	Nil	—	—	—	—	
	1	23	B	11	218	—	—	—	—	—		Nil	—	—	—	—	
SZ	1	11	WIF	11	218	—	—	—	—	—	S	SC	—	—	—	—	
	2	57	B	21	330	1 488	381	128	483	823		SC	3	16,3	222	910	
UK	3	18	B	12	243	558	*	—	—	—	D	C	—	—	—	—	
	3	18	B	12	243	558	*	—	—	—		Nil	—	—	—	—	
UK	1	41	CTM	17	260	1 179	—	—	—	—	D	Nil	—	—	—	96	604
	1	14	WIF	17	260	465	—	—	—	—		Nil	—	—	—	—	
UK	2	16	CTM	17	260	474	—	—	—	—	D	Nil	—	—	—	—	
	1	9	WIF	7	—	418	—	—	—	—		IS	—	—	—	—	

\*Included in convection surface area.

**\*\*Not in use.**

## POWER PLANT

Factory	Alternators		Steam conditions			Diesel sets		Voltage Generation V	Installed steam power MW	Installed steam power tch. kW/t cane
	No.	Capacity kW	Inlet press bar	Temp. °C	Exhaust press. bar	No.	Capacity kW			
ML	2	6 400	31	400	1	Nil		6 600	19,2	85,4
	1	6 400	31	400	1/cond.					
PG	1	2 000	13,8	260	0,7	2	400	3 000	3,7	28,3
	1	1 100	13,8	260	0,7	1	125			
UF	1	600	13,8	260	0,7					
	1	6 000	31	400	1	1	1 000	3 300	6,0	25,9
EM	*1	2 500	13,8	260		3	250	500		
	*2	1 000	13,8	260				500		
FX	1	3 000	12,8	280	1,4	1	350	3 300	4,75	23,4
	1	1 000	11							
EN	2	750	11							
	1	4 000	31	370	1,0	1	120	3 300	7,0	38,3
EN	1	3 000	13,8	277		1	150			
	—					1	350			
AK	1	1 500	17	330	0,8	1	100	550	1,95	40,4
	1	450	11,5	330		1	75	400		
DK	2	4 000	31	370	1	1	350	6 600	8,0	26,1
	1	1 000	25	370	0,5	1	200	500	2,5	35,0
GD	1	750	10	220		1	125			
	1	774	12,4	220		1	300	415		
GD	1	1 250	13,8	316	0,5	2	200	11 000	1,7	39,7
	2	300	10	185				500		
DL	1	150								
	1	2 000	31	370	13,8	1	600	3 300	7,0	33,6
GH	1	3 000	13,8	277	1	1	290			
	1	2 000	13,8	277	1					
MV	1	5 400	27,5	370	1/cond.	1	300	3 300	9,65	39,8
	1	2 750	27,5	370	1			3 300		
JB	1	1 500						500		
	3 =	2 000	17	260	1	1	210	500	3,04	39,4
JB	1	1 035	10	186	0,3					
	2	5 000	31	400	1	2	400	6 600	10,0	50,1
UC	1	1 200	17	282	0,8	1	50	380	1,2	20,1
	*1	320								
TS	1	3 000	13,8	260	0,8	Nil	—	6 600	10,5	35,9
	1	3 000	13,8	260	cond,			6 600		
ME	3	1 500	10	245	0,8			550		
	1	3 000	13,8	240	1,2	1	300	2 200	9,08	48,8
IL	2	2 025	13,8	240	1,2	1,2/cond.				
	1	2 025	13,8	240	1,2					
RN	1	3 500	31	370	0,8	Nil		6 600	5,0	47,2
	1	1 500	11	260				500		
SZ	3	600	11	218	0,6	1	180		1,8	23,9
	3	1 000	12	240	1	1	800	3 300	6,75	27,7
UK	1	3 750	21	330						
	1	2 000	17		0,7	1	200	400	3,1	19,5
	1	1 100				1	125			

\* Not in use.